

4/21/2006

**University of Portland  
School of Engineering**

**EE 301-Electromagnetic Fields-3 cr. hrs.  
Spring 2006**

**Midterm Exam # 2**

**Sinusoidal Steady-State Waves on Transmission Lines**

(Prepared by Professor A. S. Inan)

(Friday, April 21, 2006)

(Closed Book Exam; 2 Formula Sheets Allowed)

(Total Time: 55 mins.)

Name: S L U N S ☺

Signature: [Handwritten Signature] ☺

*"Honesty is the best policy"*  
Aesop (~ 620B.C.?)

*"An honest mind possesses a kingdom."*  
Lucius Annaeus Seneca (4B.C.-65A.D.)

*"Honest people are the true winners of the universe."*  
Anonymous

*"Honesty is not for sale."*  
A. Inan



Inan said I can use the Smith Chart if I choose to do so!


This is a good sign, it shows that Inan is leaning more towards democracy. I heard that in the past that there were times when he banned the use of Smith Charts!

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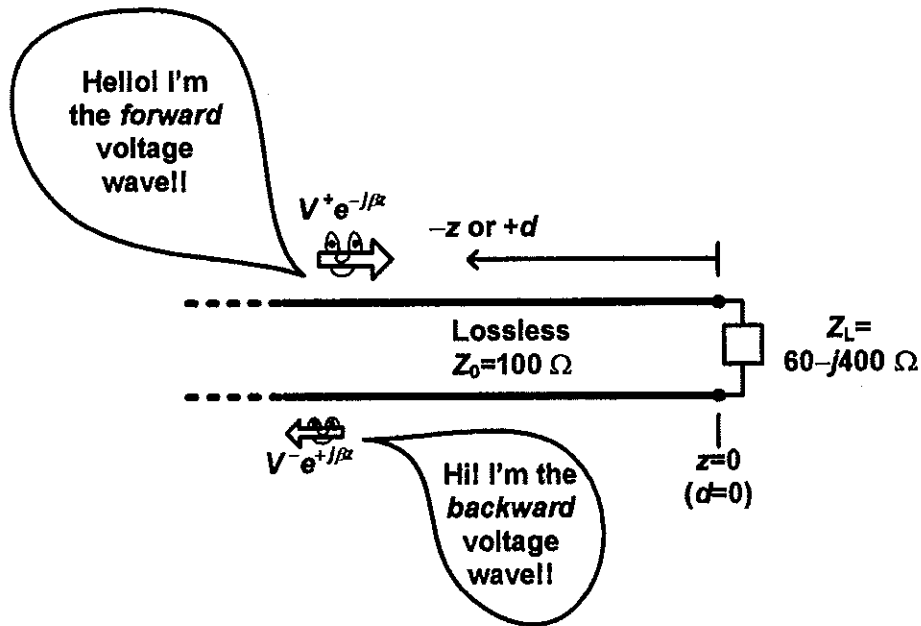
This table will be used by Inan for grading!

Problem #	Points gained
#1	
#2	
#3	
Total	

However, it's still hard to predict Inan's Time will show what he's going to do next?



(1) (15 mins., Total: 40 points) A lossless transmission line terminated with a complex impedance. A  $100\ \Omega$  transmission line is terminated with an inductive load impedance given by  $Z_L = 60 - j400\ \Omega$ , as shown.

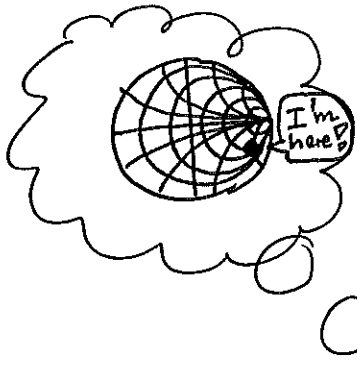


(a) (10 points) Find the load reflection coefficient,  $\Gamma_L$ . (Provide your answer in polar form.) Show your work!

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{60 - j400 - 100}{60 - j400 + 100} = \frac{-40 - j400}{160 - j400}$$

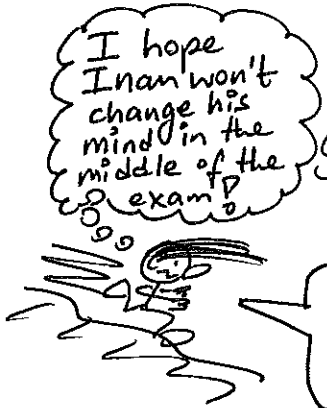
$$= \frac{-1 - j10}{4 - j10} \times \frac{4 + j10}{4 + j10} = \frac{96 - j50}{4^2 + (10)^2}$$

$$\approx 0.933 e^{-j27.5^\circ}$$



Even if I'm not using the Smith chart, I know where  $\Gamma_L$  is on the Smith Chart!

(b) (10 points) What is the value of the standing wave ratio,  $S$ , on the line? (Show your work!)



$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|} \approx \frac{1 + 0.933}{1 - 0.933} \approx \boxed{28.9}$$

And it's a big relief to know that I can use it if I want to!

(c) (10 points) Calculate the percentage time-average incident power that reflects back from the load.

$$\begin{aligned} \text{\% power incident that reflects back} &= |\Gamma|^2 \times 100 \\ &\approx (0.933)^2 \times 100 \\ &\approx \boxed{87.1\%} \end{aligned}$$

Only ~13% of the incident power is delivered to the load!

(d) (10 points) Find the  $V_{\max}$  and  $V_{\min}$  positions nearest to the load. Provide your answers as electrical lengths.

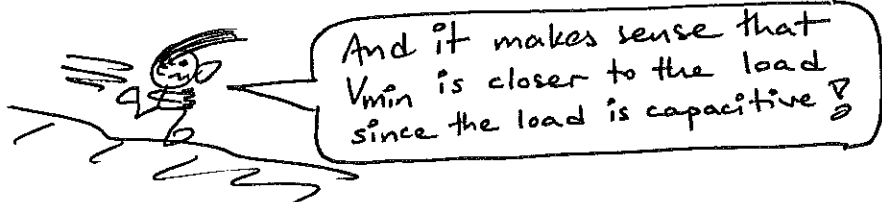
I've to convert into radians!

$$\phi_L + 2\beta z_{\min} = -\pi$$

I'm in radians!

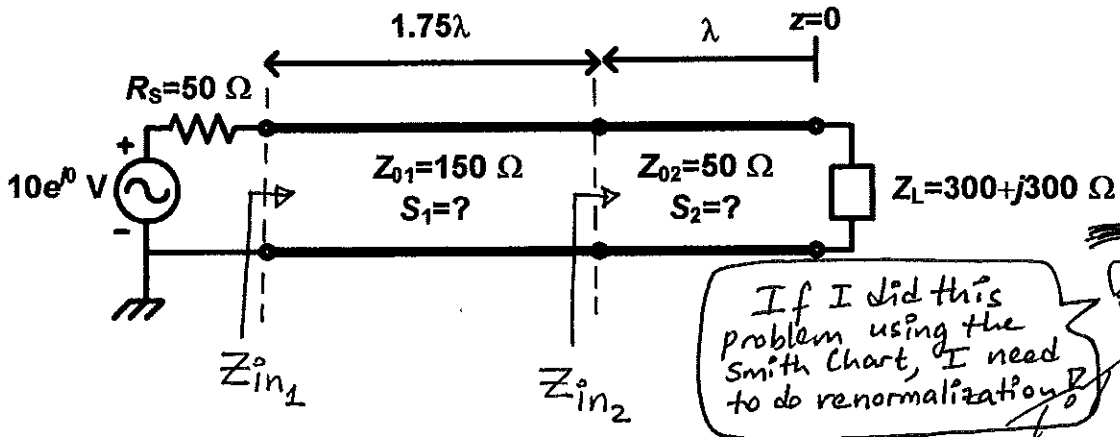
$$\rightarrow -\frac{27.5^\circ \times \pi}{180^\circ} + 4\pi \left( \frac{z_{\min}}{\lambda} \right) = -\pi$$

$$\rightarrow \frac{z_{\min}}{\lambda} \approx \boxed{-0.212} \rightarrow \frac{z_{\max}}{\lambda} = \frac{z_{\min}}{\lambda} - 0.25 \approx \boxed{-0.462}$$



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(2) (15 mins., Total: 30 points) Two cascaded transmission lines. Consider the transmission line circuit as shown. Assume lossless lines.



(a) (15 points) Find the standing wave ratio on each line. Show your work!

$$\Gamma_L = \frac{Z_L - Z_{02}}{Z_L + Z_{02}} = \frac{300 + j300 - 50}{300 + j300 + 50} = \frac{250 + j300}{350 + j300}$$

$$= \frac{5 + j6}{7 + j6} \times \frac{7 - j6}{7 - j6} = \frac{71 + j12}{(7)^2 + (6)^2} \approx 0.847e^{j9.59^\circ}$$

$$\therefore S_2 = \frac{1 + |\Gamma_L|}{1 - |\Gamma_L|} \approx \frac{1 + 0.847}{1 - 0.847} \approx \boxed{12.1}$$

Note that  $Z_{in2} = Z_L = 300 + j300 \Omega$  since the second line's length is  $\lambda$ .

$$\Gamma_{in2} = \frac{Z_{in2} - Z_{01}}{Z_{in2} + Z_{01}} = \frac{300 + j300 - 150}{300 + j300 + 150} = \frac{1 + j2}{3 + j2} \times \frac{3 - j2}{3 - j2}$$

$$= \frac{7 + j4}{13} \approx 0.620e^{j29.7^\circ}$$

$$\therefore S_1 = \frac{1 + |\Gamma_{in2}|}{1 - |\Gamma_{in2}|} \approx \frac{1 + 0.62}{1 - 0.62} \approx \boxed{4.27}$$

If I did this problem using the Smith Chart, I need to do renormalization.



$S_2 > S_1$

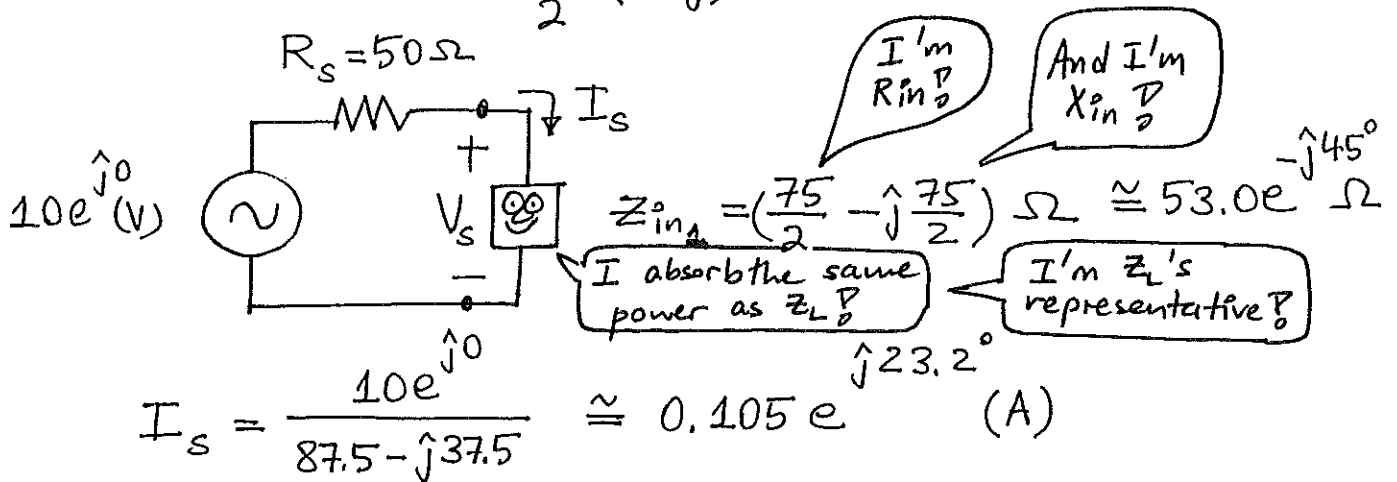
More reflections on line 2 than line 1

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(b) (15 points) Find the time-average power delivered to the load impedance.

Since the length of the first line is  $1.75\lambda$ , then,  $Z_{in_1}$  can be found as

$$Z_{in_1} = \frac{Z_{o1}^2}{Z_{in_2}} = \frac{(150)^2}{300 + j300} = \frac{75}{1+j} \times \frac{1-j}{1-j}$$
$$= \frac{75}{2} (1-j) \Omega$$



∴ Power delivered to  $Z_{in_1}$  can be calculated as

$$P_{Z_{in_1}} = \frac{1}{2} |I_s|^2 |Z_{in_1}| \cos(\angle Z_{in_1})$$
$$\approx \frac{1}{2} (0.105)^2 (53) \cos(-45^\circ) \approx 0.207 \text{ W}$$

∴ Since both transmission lines are lossless, then,

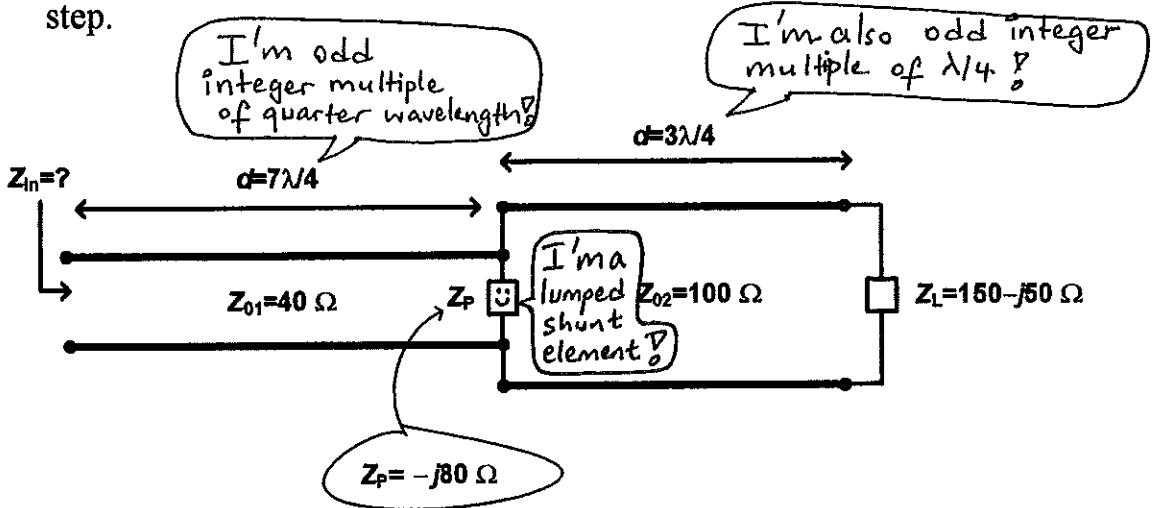
$$P_L = P_{Z_{in_1}} \approx \boxed{0.207 \text{ W}}$$

This power is dissipated by the  $R_{in}$  part of  $Z_{in}$

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(3) (15 mins., Total: 30 points) **Input impedance.** Consider the transmission line circuit as shown where  $Z_p$  impedance represents a parallel lumped element.

(a) (20 points) Find the input impedance  $Z_{in}$ . Show your work step by step.



$$Z_{in_2} = \frac{Z_{02}^2}{Z_L} = \frac{(100)^2}{150 - j50} = \frac{200}{3 - j} \times \frac{3 + j}{3 + j}$$

$$= 20(3 + j) = 60 + j20 \Omega.$$

$$Z_p \parallel Z_{in_2} = \frac{(-j80)(60 + j20)}{-j80 + 60 + j20} = \frac{(-j80)(3 + j)}{3(1 - j)} \times \frac{1 + j}{1 + j}$$

$$= -\frac{j40}{3} (2 + j4) = \frac{160 - j80}{3} \Omega$$

$$\therefore Z_{in_1} = \frac{Z_{01}^2}{Z_{eq}} = \frac{(40)^2 \times 3}{160 - j80} = \frac{60}{2 - j} \times \frac{2 + j}{2 + j}$$

$$= \frac{60(2 + j)}{5} = \boxed{24 + j12 \Omega}$$

I know how to convert  $\bar{Z}$  to  $\bar{Y}$  or  $\bar{Y}$  to  $\bar{Z}$  on the Smith Chart?

If I did this problem using the Smith Chart, I would use it as an admittance chart since  $Z_p$  is a shunt element?

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(b) (10 points) Assume that the physical length of each transmission line stays the same, however, the wavelength reduces by a factor of 2. What will be the new value of the input impedance  $Z_{in}$ ? Why? (Assume the values of  $Z_L$ ,  $Z_P$ ,  $Z_{01}$  and  $Z_{02}$  to stay the same.)

$$\text{Then, } d_1 = \frac{7\lambda_2}{2} \quad \& \quad d_2 = \frac{3\lambda_2}{2} \quad \text{where } \lambda_2 = \frac{\lambda_1}{2}.$$

$$\therefore Z_{in_2} = Z_L = 150 - j50 \Omega.$$

$$\therefore Z_{eq} = Z_P \parallel Z_{in_2} = \frac{(-j80)(150 - j50)}{150 - j130} \times \frac{15 + j13}{15 + j13}$$

$$= \frac{(-j8)(50)(3 - j)(15 + j13)}{(15)^2 + (13)^2}$$

$$= \frac{(-j400)(58 + j24)}{\underbrace{(15)^2 + (13)^2}_{394}} = \frac{4800 - j11,600}{197}$$

$$\approx \boxed{24.4 - j58.9 \Omega}$$



Both transmission lines become invisible since their lengths are integer multiples of half wavelength.

I will let you know just before the final exam starts!



And thanks Inan for letting us use the Smith Chart if we want to! Can we also use it in the final exam?