Introduction Model Verification

# Entropy model for granular materials at the critical state

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The Critical State in Geomechanics

Bi-axial compression of a 2D disk assembly:





Questions:

• At a micro-scale, is anything unusual at the critical state?

Can we predict micro-scale statistics of fabric?
 Yes, using a MaxEnt principle.



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Introduction	Critical State
Model	Questions
Verification	Scope and Objectives

# Scope and Objectives

- Focus: Contact forces, movements, and orientations at the critical state.
- 2D materials only. Biaxial loading conditions.
- Six contact quantities

 Objective: Probability density distributions of these quantities

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Contact model:

- We focus on the contacts, ignoring the particles
- No contact elasticity a purely rigid-frictional model
- No application of affine fields no static or kinematic hypotheses
- No presumed anisotropy
- A flow model contacts are either sliding or non-sliding

The model assumes isochoric critical state flow. We rely upon shearing deformation to drive the contact movements and to generate anisotropy.

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Contact model		

Rigid-frictional contact restrictions:

 $g_k^{\mathsf{n}} \in \mathbb{R}^+$ Contact sliding  $g_k^{\mathsf{t}} \in \begin{cases} -\mu g_k^{\mathsf{n}} & \Leftarrow & \dot{n}_k - \dot{\phi}_k < 0\\ (-\mu g_k^{\mathsf{n}}, \mu g_k^{\mathsf{n}}) & \Rightarrow & \dot{n}_k - \dot{\phi}_k = 0\\ \mu g_k^{\mathsf{n}} & \Leftarrow & \dot{n}_k - \dot{\phi}_k > 0 \end{cases}$ 

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#### Probability density function of the six contact quantities:

$$p(\cdots) = p(f^n, f^t, \theta^c, \theta^\ell, \dot{n}, \dot{\phi})$$

This probability density must conform to certain constraints

$$\int \cdots \int \Gamma_i(\cdots) p(\cdots) = \overline{\Gamma}_i$$
  
{ $f^n, f^t, \theta^c, \theta^\ell, \dot{n}, \dot{\phi}$ }



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Constraint #1		

#### Constraint #1: mean stress = $p_0$

$$\int \cdots \int f^{n} p(\cdots) = 2p_{0}\overline{\ell} \left(\frac{M}{A}\right)^{-1}$$

$$\{f^{n}, f^{t}, \theta^{c}, \theta^{\ell}, \dot{n}, \dot{\phi}\}$$

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# Constraint #2: frictional dissipation at the contacts must be consistent with the stress-work

$$\frac{1}{A}\sum f_{k}^{t} \overline{\ell} \left( \dot{n}_{k} - \dot{\phi}_{k} \right) = \boldsymbol{\sigma} : \mathbf{D} \quad \text{with} \quad \mathbf{D} = \begin{bmatrix} -\dot{\varepsilon} & \mathbf{0} \\ \mathbf{0} & \dot{\varepsilon} \end{bmatrix}$$

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$$\begin{cases} \int \cdots \int \left[ f^{t}(\dot{n}_{k} - \dot{\phi}_{k}) + \dot{\varepsilon}f^{n}(-\cos^{2}\theta^{c} + \sin^{2}\theta^{c}) - \dot{\varepsilon}f^{t}(-2\cos\theta^{c}\sin\theta^{c}) \right] p(\cdots) = 0 \end{cases}$$

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Constraint #2: frictional dissipation at the contacts must be consistent with the stress-work

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or

$$\int \cdots \int \left[ f^{\mathsf{t}}(\dot{n}_{k} - \dot{\phi}_{k}) + \dot{\varepsilon} f^{\mathsf{n}}(-\cos^{2}\theta^{\mathsf{c}} + \sin^{2}\theta^{\mathsf{c}}) - \dot{\varepsilon} f^{\mathsf{t}}(-2\cos\theta^{\mathsf{c}}\sin\theta^{\mathsf{c}}) \right] p(\cdots) = 0$$

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Constraint #3			

#### Constraint #3: isochoric flow

$$tr(\mathbf{D}) = 0$$

or

 $\int \cdots \int \mathcal{K}(\theta^{c}, \theta^{\ell}) \dot{n} (\sin \theta^{c} \sin \theta^{\ell} + \cos \theta^{c} \cos \theta^{\ell}) p(\cdots) = 0$ { $f^{n}, f^{t}, \theta^{c}, \theta^{\ell}, \dot{n}, \dot{\phi}$ }

$$\mathcal{K}( heta^{\mathsf{c}}, heta^{\ell}) = egin{cases} rac{1}{2} - rac{1}{2\pi} \mathsf{mod}( heta^{\ell} - heta^{\mathsf{c}}, 2\pi) & heta^{\ell} 
eq heta^{\mathsf{c}} \ 0 & heta^{\ell} = heta^{\mathsf{c}} \ \end{pmatrix}$$

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Constraint #4			

#### Constraint #4: 11.2% of contacts are sliding (from DEM data).



Constraint #1: mean stress =  $p_0$ 

$$\int \cdots \int f^{n} p(\cdots) = 2p_{o}\overline{\ell} \left(\frac{M}{A}\right)^{-1}$$
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Disorder	

The Shannon entropy associated with the probability density:

$$H\{p(\cdots)\} = -\int \cdots \int p(\cdots) \ln(p(\cdots)) + \{f^{\mathsf{n}}, f^{\mathsf{t}}, \theta^{\mathsf{c}}, \theta^{\ell}, \dot{n}, \dot{\phi}\}$$

The density  $p(\dots)$  with the largest entropy corresponds to the most likely "macro-state" and encompasses the broadest combination of the 6 contact quantities.

Must maximize H subject to the constraints #1, #2, #3, and #4.

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Entropy H is maximized with the following probability density:

$$p(\cdots) = \frac{1}{Z(\cdots)} \exp\left(-\sum_{i=1}^{4} \lambda_i \Gamma_i(\cdots)\right)$$

where the  $\Gamma_i$  are Lagrange multipliers, and the  $\Gamma_i(\cdots)$  functions.

For example,

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Anisotropy of contact forces:



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	Introduction Model Verification	Anisotropy Force density distribution Weak & strong contacts
Normal forces		

Probability density of the normal contact forces:



# Weak-strong contacts

Contribution of contacts to the bulk deviatoric stress.

Other investigators have found that the most heavily loaded contacts account for nearly the entire deviatoric stress.





- The critical state is characterized by a maximum disorder model
- The disorder model predicts fabric anisotropy reasonably well.
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Questions?		

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